## **Appendix: Orthogonal Curvilinear Coordinates**

## Notes:

Most of the material presented in this chapter is taken from Anupam, G. (Classical Electromagnetism in a Nutshell 2012, (Princeton: New Jersey)), Chap. 2, and Weinberg, S. (Gravitation and Cosmology: Principles and Applications of the General Theory of Relativity 1972, (Wiley: New York), Chap. 8.

We define the infinitesimal spatial displacement vector  $d\mathbf{x}$  in a given orthogonal coordinate system with

$$d\mathbf{x} = dx^{i}\mathbf{e}_{i}, \tag{II.1}$$

where the Einstein summation convention was used,  $dx^i$  is a contravariant component and  $\mathbf{e}_i$  is a basis vector (*i* = 1,2,3). The length interval *ds* is thus given by

$$ds^{2} = d\mathbf{x} \cdot d\mathbf{x}$$

$$= (dx^{i} \mathbf{e}_{i}) \cdot (dx^{j} \mathbf{e}_{j})$$

$$= (\mathbf{e}_{i} \cdot \mathbf{e}_{j}) dx^{i} dx^{j}$$

$$= g_{ij} dx^{i} dx^{j}$$

$$= dx^{i} dx_{i},$$
(II.2)

where the orthogonality of the coordinate system is specified by  $\mathbf{e}_i \cdot \mathbf{e}_j = g_{ij}$  with the metric tensor  $g_{ij} = 0$  when  $i \neq j$ , and  $dx_i$  is the covariant component. Please note that basis vectors are not unit vectors, i.e.,  $\mathbf{e}_i \cdot \mathbf{e}_i \neq 1$  in general. Equation (II.2) can be used to similarly define the inner product between any two vectors with

$$\mathbf{A} \cdot \mathbf{B} = g_{ij} A^i B^j$$
  
=  $A^i B_i$ . (II.3)

Since the covariant and contravariant components are generally different from one another in non-Cartesian coordinate systems, it is often more desirable to introduce a new set of so-called *ordinary* or *physical components* that preserve the inner product without explicitly bringing in both types of components or the metric tensor.

We start by rewriting equation (II.2) as

$$ds^{2} = (h_{1}du^{1})^{2} + (h_{2}du^{2})^{2} + (h_{3}du^{3})^{2}$$
(II.4)

for the orthogonal coordinate system  $(u^1, u^2, u^3)$ . A comparison with equation (II.2) reveals that  $h_i^2 = g_{ii}$ . For example, Cartesian coordinates have  $h_1 = h_2 = h_3 = 1$ , cylindrical coordinates  $(\rho, \theta, z)$  have  $h_1 = h_3 = 1$ ,  $h_2 = \rho$ , and spherical coordinates  $(r, \theta, \phi)$  have  $h_1 = 1$ ,  $h_2 = r$ , and  $h_3 = r\sin(\theta)$ . Going back to equation (II.3) for the inner product, we now define the physical coordinates  $\overline{A}_i$  of a vector **A** such that

$$\mathbf{A} \cdot \mathbf{B} \equiv \overline{A}_i \overline{B}_i, \tag{II.5}$$

where the use of subscripts has no particular meaning (i.e., a subscript does not imply a covariant component). A comparison with equation (II.3) implies that the physical components are related to the covariant and contravariant components through

$$\overline{A}_i = h_i A^i = h_i^{-1} A_i. \tag{II.6}$$

The first thing we should notice is that the physical components allow the use of a unit basis  $\hat{\mathbf{e}}_i$  since

$$\mathbf{e}_{i} \cdot \mathbf{e}_{j} = g_{ij}$$

$$= h_{i}h_{j}\delta_{ij}$$

$$= h_{i}h_{j}\left(\hat{\mathbf{e}}_{i} \cdot \hat{\mathbf{e}}_{j}\right)$$

$$= (h_{i}\hat{\mathbf{e}}_{i}) \cdot (h_{j}\hat{\mathbf{e}}_{j}).$$
(II.7)

In fact, we could have alternatively justified the introduction of the physical components by the desire to use a unit basis with

$$d\mathbf{x} = h_1 du^1 \hat{\mathbf{e}}_1 + h_2 du^2 \hat{\mathbf{e}}_2 + h_3 du^3 \hat{\mathbf{e}}_3$$
  
=  $d\overline{x}_1 \hat{\mathbf{e}}_1 + d\overline{x}_2 \hat{\mathbf{e}}_2 + d\overline{x}_3 \hat{\mathbf{e}}_3$  (II.8)

or in general

$$\mathbf{A} = \overline{A}_1 \hat{\mathbf{e}}_1 + \overline{A}_2 \hat{\mathbf{e}}_2 + \overline{A}_3 \hat{\mathbf{e}}_3. \tag{II.9}$$

It should now be clear that what we usually specify as *coordinates* (e.g.,  $(\rho, \theta, z)$  and  $(r, \theta, \phi)$ ) correspond to the contravariant components of  $d\mathbf{x}$ , while the *physical* coordinates are those for which the components of  $d\mathbf{x}$  have units of length (e.g.,  $(d\rho, \rho d\theta, dz)$  and  $(dr, rd\theta, r\sin(\theta) d\phi)$ ).

We now define the different differential operators using the physical coordinates, starting with the gradient. To do so, we first consider the differential of a scalar function f

$$df = \frac{\partial f}{\partial u^{i}} du^{i}$$
  

$$\equiv \nabla f \cdot d\mathbf{x}$$
  

$$= \nabla f \cdot \left(\sum_{i} h_{i} du^{i} \hat{\mathbf{e}}_{i}\right)$$
  

$$= \sum_{i} h_{i} du^{i} \nabla f \cdot \hat{\mathbf{e}}_{i},$$
  
(II.10)

which from the first and last equations implies that

$$\nabla f = \frac{1}{h_1} \frac{\partial f}{\partial u^1} \hat{\mathbf{e}}_1 + \frac{1}{h_2} \frac{\partial f}{\partial u^2} \hat{\mathbf{e}}_2 + \frac{1}{h_3} \frac{\partial f}{\partial u^3} \hat{\mathbf{e}}_3.$$
(II.11)

This leads to the following relations for the cylindrical and spherical coordinate systems

$$\nabla f = \frac{\partial f}{\partial \rho} \hat{\mathbf{e}}_{\rho} + \frac{1}{\rho} \frac{\partial f}{\partial \theta} \hat{\mathbf{e}}_{\theta} + \frac{\partial f}{\partial z} \hat{\mathbf{e}}_{z}$$

$$\nabla f = \frac{\partial f}{\partial r} \hat{\mathbf{e}}_{r} + \frac{1}{r} \frac{\partial f}{\partial \theta} \hat{\mathbf{e}}_{\theta} + \frac{1}{r \sin(\theta)} \frac{\partial f}{\partial \phi} \hat{\mathbf{e}}_{\phi},$$
(II.12)

respectively. For the divergence of a vector we consider an infinitesimal cube, as shown in Figure 1, and use the divergence theorem



**Figure 1** - Infinitesimal volume of integration, where we do not differentiate between  $du^i$  and  $du_i$ .

$$\int_{V} \nabla \cdot \mathbf{A} d^{3} x = \nabla \cdot \mathbf{A} h_{1} h_{2} h_{3} du^{1} du^{2} du^{3}$$
  
=  $\int_{S} \mathbf{A} \cdot \mathbf{n} da$ , (II.13)

which for a small enough cube we can write as

$$\int_{S} \mathbf{A} \cdot \mathbf{n} \, da = \left[ \overline{A}_{1} h_{2} h_{3} \right]_{\text{right}}^{\text{left}} du^{2} du^{3} + \left[ \overline{A}_{2} h_{1} h_{3} \right]_{\text{back}}^{\text{front}} du^{1} du^{3} + \left[ \overline{A}_{3} h_{1} h_{2} \right]_{\text{bottom}}^{\text{top}} du^{1} du^{2} = \left[ \frac{\partial}{\partial u^{1}} \left( \overline{A}_{1} h_{2} h_{3} \right) + \frac{\partial}{\partial u^{2}} \left( \overline{A}_{2} h_{1} h_{3} \right) + \frac{\partial}{\partial u^{3}} \left( \overline{A}_{3} h_{1} h_{2} \right) \right] du^{1} du^{2} du^{3},$$
(II.14)

since in general  $h_i$  can vary across the dimensions of the cube. A comparison with equation (II.13) reveals that

$$\nabla \cdot \mathbf{A} = \frac{1}{h_1 h_2 h_3} \left[ \frac{\partial}{\partial u^1} \left( \overline{A}_1 h_2 h_3 \right) + \frac{\partial}{\partial u^2} \left( \overline{A}_2 h_1 h_3 \right) + \frac{\partial}{\partial u^3} \left( \overline{A}_3 h_1 h_2 \right) \right].$$
(II.15)

We then respectively have for cylindrical and spherical coordinates

$$\nabla \cdot \mathbf{A} = \frac{1}{\rho} \frac{\partial}{\partial \rho} (\rho \overline{A}_r) + \frac{1}{\rho} \frac{\partial \overline{A}_{\theta}}{\partial \theta} + \frac{\partial \overline{A}_z}{\partial z}$$

$$\nabla \cdot \mathbf{A} = \frac{1}{r^2} \frac{\partial}{\partial r} (r^2 \overline{A}_r) + \frac{1}{r \sin(\theta)} \frac{\partial}{\partial \theta} (\sin(\theta) \overline{A}_{\theta}) + \frac{1}{r \sin(\theta)} \frac{\partial \overline{A}_{\phi}}{\partial \phi}.$$
(II.16)

The Laplacian is readily evaluated by setting  $\mathbf{A} = \nabla f$  and inserting equations (II.12) in equations (II.16). We then have the corresponding relations

$$\nabla^{2} f = \frac{1}{\rho} \frac{\partial}{\partial \rho} \left( \rho \frac{\partial f}{\partial \rho} \right) + \frac{1}{\rho^{2}} \frac{\partial^{2} f}{\partial \theta^{2}} + \frac{\partial^{2} f}{\partial z^{2}}$$

$$\nabla^{2} f = \frac{1}{r^{2}} \frac{\partial}{\partial r} \left( r^{2} \frac{\partial f}{\partial r} \right) + \frac{1}{r^{2} \sin(\theta)} \frac{\partial}{\partial \theta} \left( \sin(\theta) \frac{\partial f}{\partial \theta} \right) + \frac{1}{r^{2} \sin^{2}(\theta)} \frac{\partial^{2} f}{\partial \phi^{2}}$$
(II.17)

for cylindrical and spherical coordinates, respectively.

Finally, for the curl we use Stokes' Theorem using an infinitesimal surface as shown in Figure 2

$$\int_{S} (\nabla \times \mathbf{A}) \cdot \mathbf{n} \, da = (\nabla \times \mathbf{A}) \cdot \left( \alpha h_{2} h_{3} du^{2} du^{3} \hat{\mathbf{e}}_{1} + \beta h_{1} h_{3} du^{1} du^{3} \hat{\mathbf{e}}_{2} + \gamma h_{1} h_{2} du^{1} du^{2} \hat{\mathbf{e}}_{3} \right)$$

$$= \oint_{C} \mathbf{A} \cdot d\mathbf{I},$$
(II.18)



**Figure 2** – Infinitesimal loop of integration for the derivation of the curl, projection in the  $(u^1, u^2)$ -plane.

where  $\mathbf{n} = \alpha \hat{\mathbf{e}}_1 + \beta \hat{\mathbf{e}}_2 + \gamma \hat{\mathbf{e}}_3$ . For this infinitesimal loop we can consider the different projections on the three  $(u^i, u^j)$ -planes and write (using the first two terms of the corresponding Taylor expansions)

$$\begin{split} \oint_{C} \mathbf{A} \cdot d\mathbf{l} &= \alpha \left\{ \left[ \overline{A}_{2} h_{2} \right]_{\text{top}}^{\text{bottom}} du^{2} + \left[ \overline{A}_{3} h_{3} \right]_{\text{back}}^{\text{front}} du^{3} \right\} \\ &+ \beta \left\{ \left[ \overline{A}_{1} h_{1} \right]_{\text{bottom}}^{\text{top}} du^{1} + \left[ \overline{A}_{3} h_{3} \right]_{\text{left}}^{\text{right}} du^{3} \right\} \\ &+ \gamma \left\{ \left[ \overline{A}_{1} h_{1} \right]_{\text{front}}^{\text{back}} du^{1} + \left[ \overline{A}_{2} h_{2} \right]_{\text{right}}^{\text{left}} du^{2} \right\} \\ &= \alpha \left[ -\frac{\partial}{\partial u^{3}} (\overline{A}_{2} h_{2}) + \frac{\partial}{\partial u^{2}} (\overline{A}_{3} h_{3}) \right] \\ &+ \beta \left[ \frac{\partial}{\partial u^{3}} (\overline{A}_{1} h_{1}) - \frac{\partial}{\partial u^{2}} (\overline{A}_{3} h_{3}) \right] \\ &+ \gamma \left[ -\frac{\partial}{\partial u^{2}} (\overline{A}_{1} h_{1}) + \frac{\partial}{\partial u^{1}} (\overline{A}_{2} h_{2}) \right]. \end{split}$$
(II.19)

Equating equations (II.18) and (II.19) we must have

$$\nabla \times \mathbf{A} = \frac{1}{h_2 h_3} \left[ \frac{\partial}{\partial u^2} (\overline{A}_3 h_3) - \frac{\partial}{\partial u^3} (\overline{A}_2 h_2) \right] \hat{\mathbf{e}}_1 + \frac{1}{h_1 h_3} \left[ \frac{\partial}{\partial u^3} (\overline{A}_1 h_1) - \frac{\partial}{\partial u^1} (\overline{A}_3 h_3) \right] \hat{\mathbf{e}}_2 + \frac{1}{h_1 h_2} \left[ \frac{\partial}{\partial u^1} (\overline{A}_2 h_2) - \frac{\partial}{\partial u^2} (\overline{A}_1 h_1) \right] \hat{\mathbf{e}}_3.$$
(II.20)

We then respectively write for the cylindrical and spherical coordinate systems

$$\nabla \times \mathbf{A} = \left[\frac{1}{\rho} \frac{\partial \overline{A}_{z}}{\partial \theta} - \frac{\partial \overline{A}_{\theta}}{\partial z}\right] \hat{\mathbf{e}}_{\rho} + \left[\frac{\partial \overline{A}_{\rho}}{\partial z} - \frac{\partial \overline{A}_{z}}{\partial \rho}\right] \hat{\mathbf{e}}_{\theta} + \frac{1}{\rho} \left[\frac{\partial}{\partial \rho} (\rho \overline{A}_{\theta}) - \frac{\partial \overline{A}_{\rho}}{\partial \theta}\right] \hat{\mathbf{e}}_{z}$$

$$\nabla \times \mathbf{A} = \frac{1}{r \sin(\theta)} \left[\frac{\partial}{\partial \theta} (\sin(\theta) \overline{A}_{\phi}) - \frac{\partial \overline{A}_{\theta}}{\partial \phi}\right] \hat{\mathbf{e}}_{r} + \left[\frac{1}{r \sin(\theta)} \frac{\partial \overline{A}_{r}}{\partial \phi} - \frac{1}{r} \frac{\partial}{\partial r} (r \overline{A}_{\phi})\right] \hat{\mathbf{e}}_{\theta} \quad (\text{II.21})$$

$$+ \frac{1}{r} \left[\frac{\partial}{\partial r} (r \overline{A}_{\theta}) - \frac{\partial \overline{A}_{r}}{\partial \theta}\right] \hat{\mathbf{e}}_{\phi}.$$